

# Development of Flexible Matrix Composites (FMC) for Fluidic Actuators in Morphing Systems

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# Outline

SADE- Project description

- Main ideas

Droop nose - concepts

- Actuation System
  - Material properties

Flexible Matrix Composites (FMC)

- Definition
- Combinations
- Production Process

Experiments

Tensile tests

Simulation

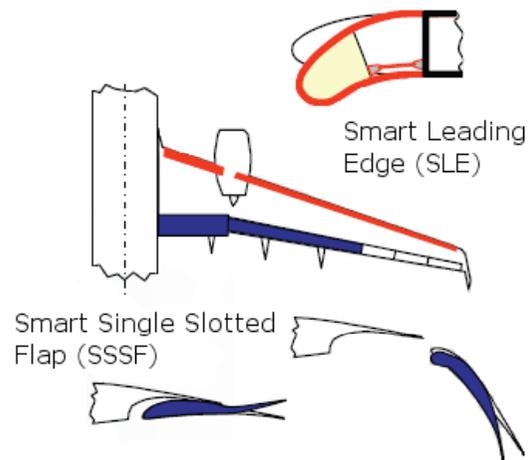
Conclusion

## SADE (Smart High Lift Devices for Next Generation Wings)

The project's aim is to create a seamless and gapless high lift device at the wing's leading and trailing edge with the goal to reduce the airframe's noise and drag and enable laminar wing flow.

Two points of focus:

- leading edge
- trailing edge



SADE smart high lift configurations  
(Source: DLR)



**This lecture: focus on leading edge in form of droop nose.**

# Drop Nose – Requirements

## Enable laminar flow

Reduce noise ← less turbulence

- the drop nose as to be a seam- and gapless device → enabler for a smooth surface (necessary for laminar flow)

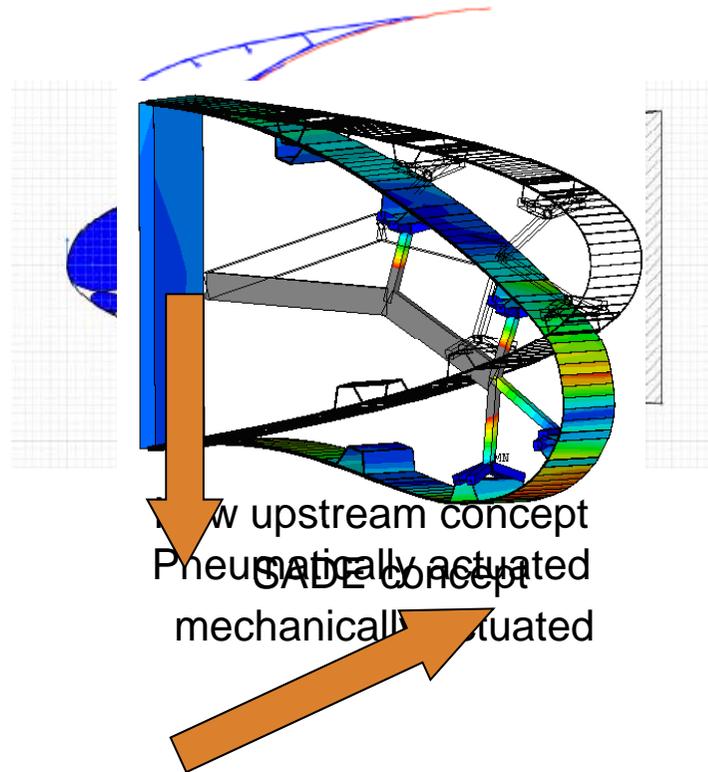
Nose material has to be

- flexible to allow the required deformation (at start and landing) and at the same time
- stiff enough to keep the needed shape.

The actuation-mechanism has to support the skin (same requirements as above)

→ to achieve good support of the skin a pneumatic actuation systems is being developed which will continuously support the skin

# Drop Nose



## Actuation Tubes

Even greater flexibility (than skin) needed, but also stiffness

- Material-requirement: flexible but also stiff

→ **Flexible matrix composites (FMC)**

Flexible matrix composites are flexible matrix materials reinforced with continuous (stiff) fibers

Goal of this study: development of a production process for FMC at “large” scale (not laboratory setting)



# Flexible matrix composites

Possible material combinations:

**Rubber, silicone and thermoplastic elastomers** with carbon or glass fibers

Table 1: Material Combinations

| Fiber Material       |                     | Matrix Material |        |          |
|----------------------|---------------------|-----------------|--------|----------|
|                      |                     | TPE             | Rubber | Silicone |
| <b>Carbon fibers</b> | Single rovings      | X               | X      |          |
|                      | UD-Tape             | X               | X      |          |
|                      | UD-non crimp fabric | X               |        |          |
|                      | Multiaxial-weave    | X               |        | X        |
| <b>Glass fibers</b>  | Multiaxial-weave    | X               |        | X        |

# Flexible matrix composites

Production techniques:

Pressure moulding, Injection moulding, Hand lamination, VAP, pultrusion

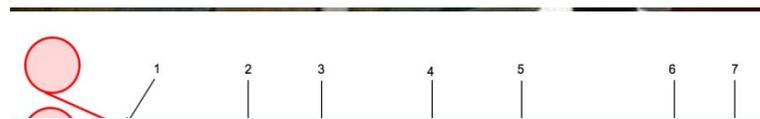


Table 2: Production processes

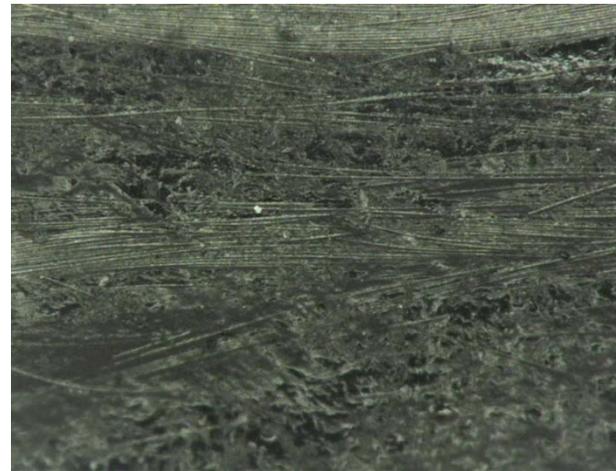
| Production method<br>Material | Hand lamination | Vacuum assisted process (VAP) | Injection moulding | Pressure moulding | Pultrusion |
|-------------------------------|-----------------|-------------------------------|--------------------|-------------------|------------|
| Rubber                        | -               | -                             | -                  | +                 | -          |
| Silicone                      | +               | -                             | -                  | -                 | -          |
| TPE                           | -               | +                             | +                  | +                 | +          |

## Experiments with rubber

Material-tests with rubber

- Production process: **pressure moulding**

Tested Material: Dynanotex HS 15/50SL (UD-tape) with rubber mixture SAA1052/70



Rubber pressed with 250-400 bar at 120°C (at Kraiburg Gummiwerke)

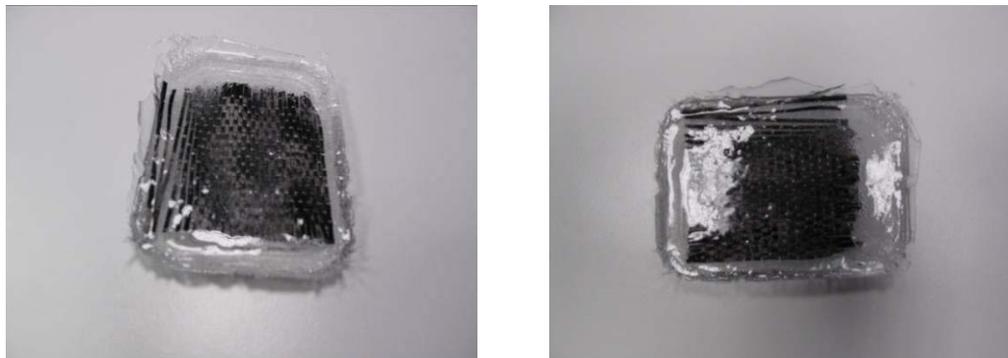
**Conclusion:** Good distribution of rubber in the fibers, but highly distorted fibers through rubber flow

## Experiments silicone rubber

Material-tests with silicone-rubber

- Production process: **hand lamination**

Tested Material: Torayca T300B 6k Biax-fabric with Wacker Elastosil LR 7665



Conclusion: Silicones have a too high viscosity to infiltrate the fibers, infiltration only possible when the silicone is diluted with e.g. benzene

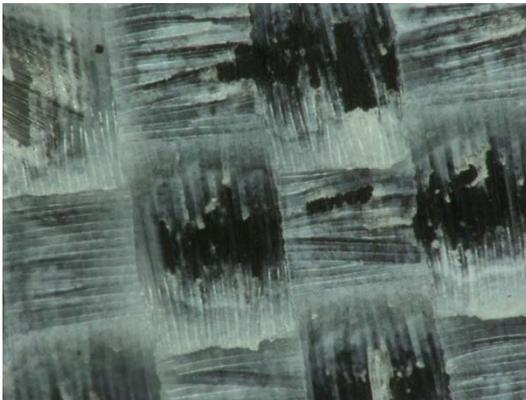
## Experiments with TPE

Material-tests with TPE

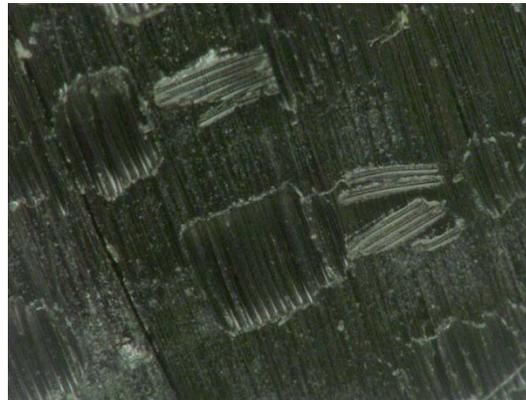
- Production process: **VAP**

Tested Material: Torayca FT 300B 6k 50B with TPE Patch HTC 8533/49

Duration: 3h at 180°C



TPE/C-Fiber laminat after VAP-process



Dry fibers (comparison)

Conclusion: TPE too viscous for VAP, very slow process, shear-forces not high enough

## Experiments with TPE

Material-tests with TPE

- Production process: **injection moulding**

Tested Material: Torayca FT 300B 6k 50B with TPE Patch HTC 8533/49



TPE/C-Fiber laminat after injection-moulding  
at 190°C into a cold cast

Conclusion: shear-forces in the nozzle reduce the viscosity, flow of the liquid TPE pushes fibers away but good through-layer infiltration, cold cast reduced spread of the TPE

# Experiments with TPE

Material-tests with TPE

- Production process: pressure moulding

Tested Material: Torayca T300B-6000 Bi-ax fabric with TPE Patch HTC 8533/49



1-layered



2-layered

TPE pressed into a biax carbon fabric at 180°C and 2.5 bar

Conclusion: Viscosity of TPEs in general low enough, pressure moulding effective but the “flow” of the TPE leads to high fiber distortions, necessary to restrict the fiber movement.

## Experiments with TPE

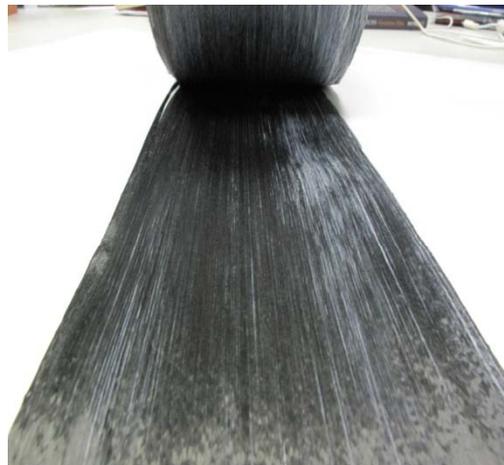
Material-tests with TPE

- Production process: **pultrusion**

Tested Material: Torayca FT 300B 6k 50B with TPE Patch HTC 8533/49



TPE/C-prepreg-Tape



4-layered TPE/C-laminat

Conclusion: Viscosity of TPEs in general low enough, pultrusion effective but the fiber-volume fraction needs to be lower in future trials

## Summary of material and production trials

| Continuous Fibers  |                                 |                |                      | Matrix Material |          |             |
|--|---------------------------------|----------------|----------------------|-----------------|----------|-------------|
| Base Material  | Fiber type                      | Fabric type    | Area weight          | TPE*            | Rubber** | Silicone*** |
| <b>Carbon Fibers</b>   | Torayca T300B-6000              | 6k-Roving      | 396 tex              | X+              | X-       |             |
|  | Dynanotex HS 15/50SL            | UD-tape        | 50 g/m <sup>2</sup>  |                 | X+       |             |
|  | Torayca T700S                   | UD-tape        | 100 g/m <sup>2</sup> | X+              |          |             |
|  | Torayca FT 300B 6k 50B          | 6k-UD-fabric   | 120 g/m <sup>2</sup> | X+              |          |             |
|  | Toho Tenax IMS65 E13 24k 830tex | 24k UD-fabric  | 208g/m <sup>2</sup>  | X-              |          |             |
|  | Torayca T300B-6000              | 6k Biax-fabric | 317 g/m <sup>2</sup> | X+              |          | X-          |
|  | Torayca T700S-12000             | 12k biax-NCF   | 578 g/m <sup>2</sup> | X-              |          | X-          |
| <b>Glass Fibers</b>  | Interglas technologies          | Biax fabric    | 288g/m <sup>2</sup>  | X-              |          | X(+)        |
| *TPE-SEBS Patch HTC 8533/49 Kraiburg TPE / **Rubber SAA1052/70 Kraiburg Gummiwerke / ***Silicone: MVQ-silicone (FSU-50-83 by MG Silikon)/ Wacker Elastosil LR 7665 |                                 |                |                      |                 |          |             |

## Preparation for Tensile Tests with FMC (C/TPE)

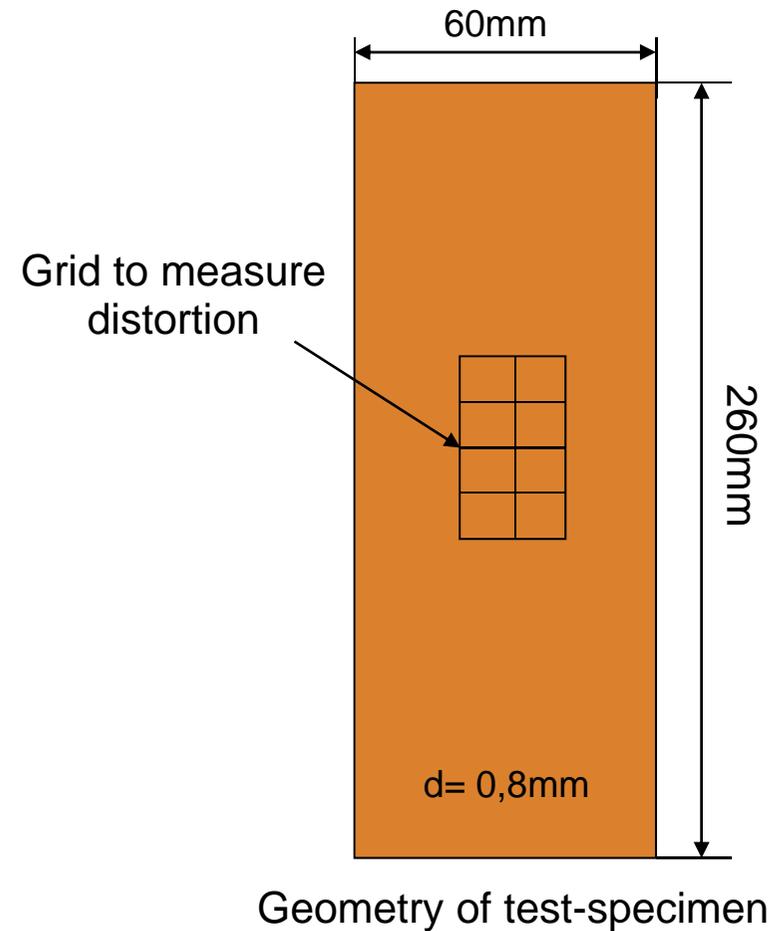
Tensile tests in  $0^\circ/90^\circ$  and  $\pm 45^\circ$  direction

8- tests/specimen each

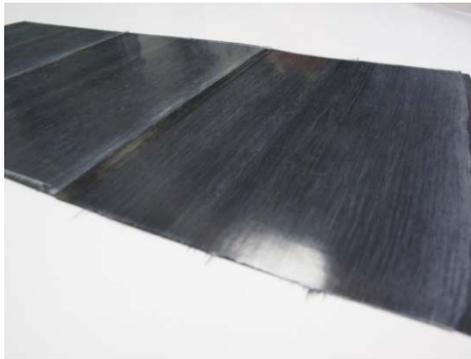
Strain measurement with optical sensor

- Only one direction possible
- For other directions: grid-deformation (recorded with video camera)

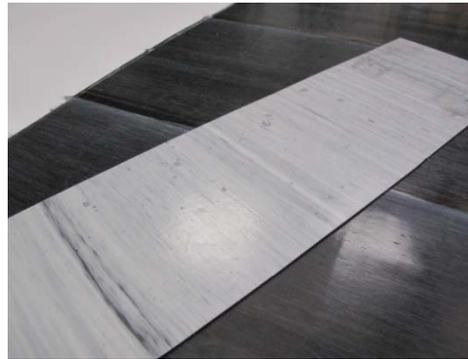
Goal: Definition of the mechanical properties for hyperelastic-anisotropic material model



## Preparation for Tensile Tests with FMC (C/TPE)



4-layered 90° laminat



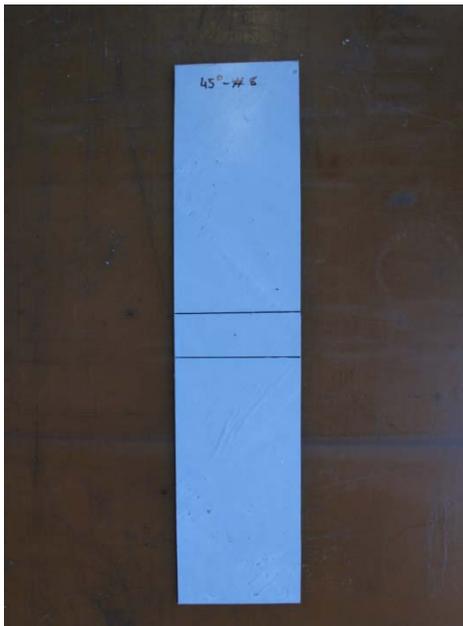
4-layered 90° laminat  
cut into specimen  
shape with an added  
TPE layer



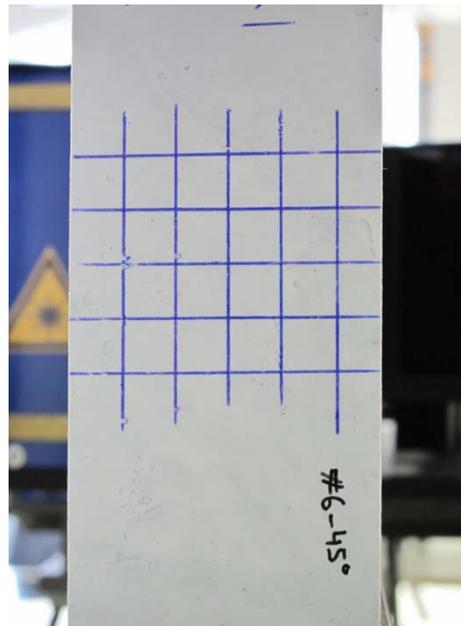
90°- specimen before  
cutting

The material from the pultrusion was used like prepreg material and stacked to create a 4 layer-thick laminat with the needed fiber-angles.

# Test-setup for Tensile Tests with FMC (C/TPE)



Test-sample



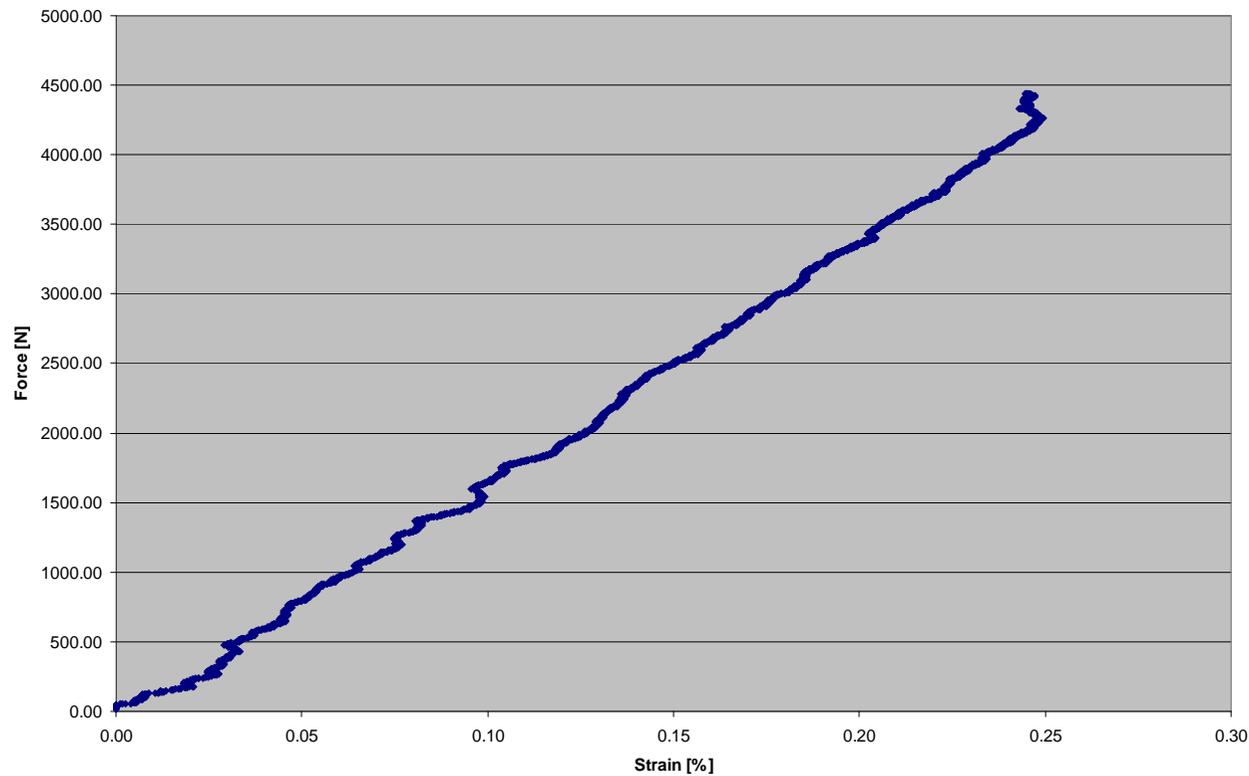
Distortion grid



Optical strain measurement

# Tensile Tests

## 0°-Results



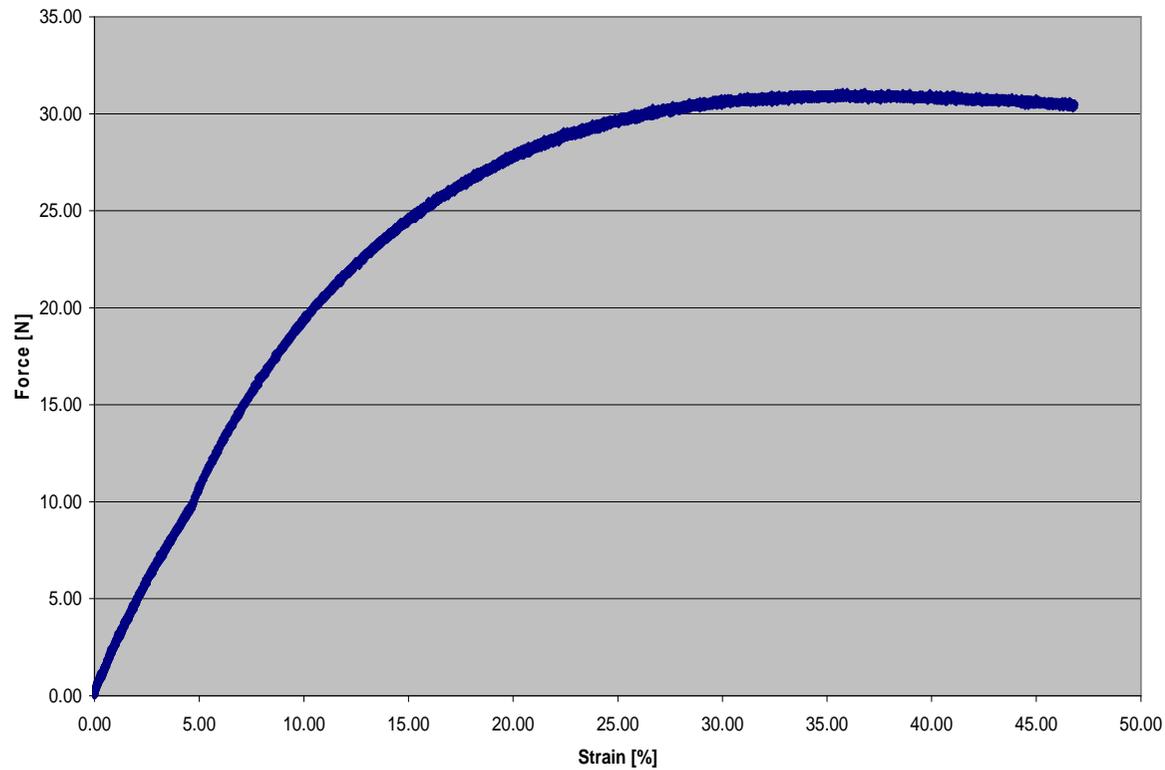
$$E_{11}=48.12 \text{ kN/mm}^2$$

In comparison to  
calculated value  
from rule of mixture  
at a fiber-volume-  
fraction of 28%

$$E_{11\text{calc}}=65\text{kN/mm}^2$$

# Tensile Tests

## 90°-Results



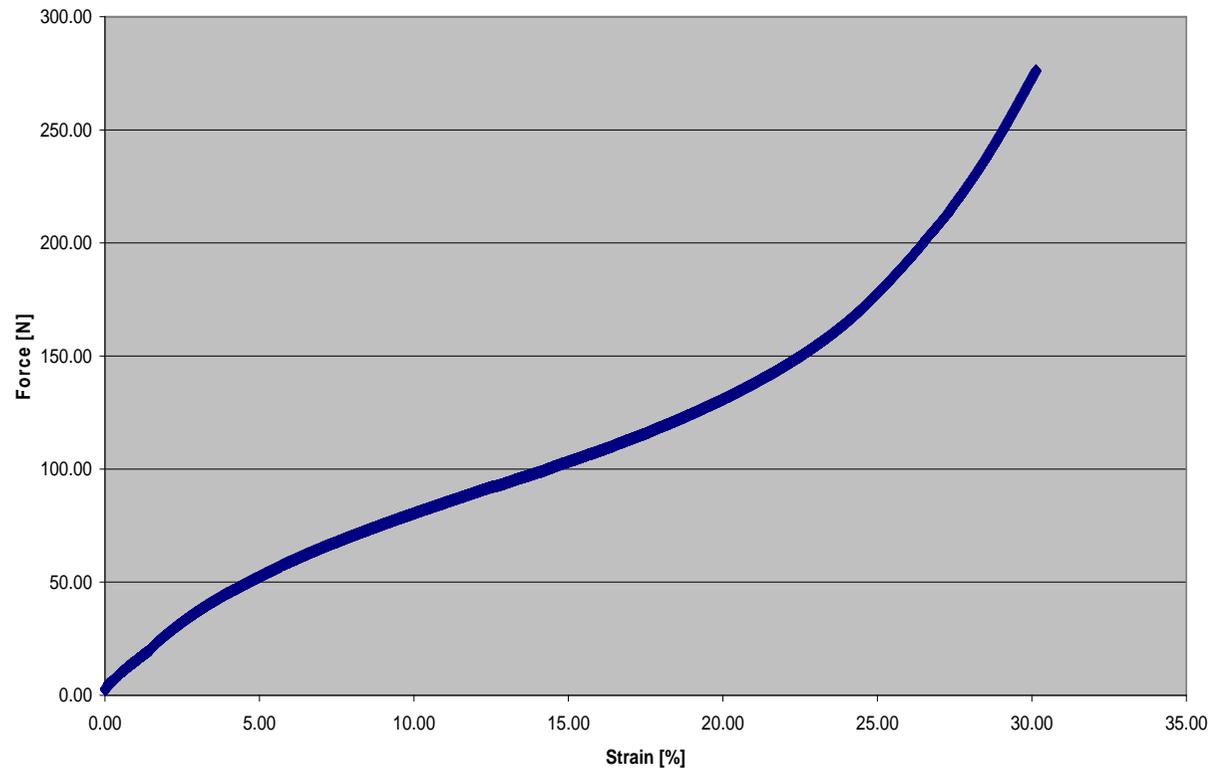
$E_{22}=6.81 \text{ N/mm}^2$   
In comparison to  
calculated value  
from rule of  
mixture at a fiber-  
volume-fraction of  
28%

$E_{11\text{calc}}=9.25\text{N/mm}^2$

only valid for  
strain less than  
3%

# Tensile Tests

## $\pm 45^\circ$ -Results



$G_{12}=17,52 \text{ N/mm}^2$   
only valid for strain less  
than 3%

At large strains (above  
25%) delaminations  
could be seen to occur  
on the edges of the  
specimen

## Tensile Tests-Results

The tests showed:

- Method for 0° -testing has to be changed.
- the different stiffness in the different directions (as expected)

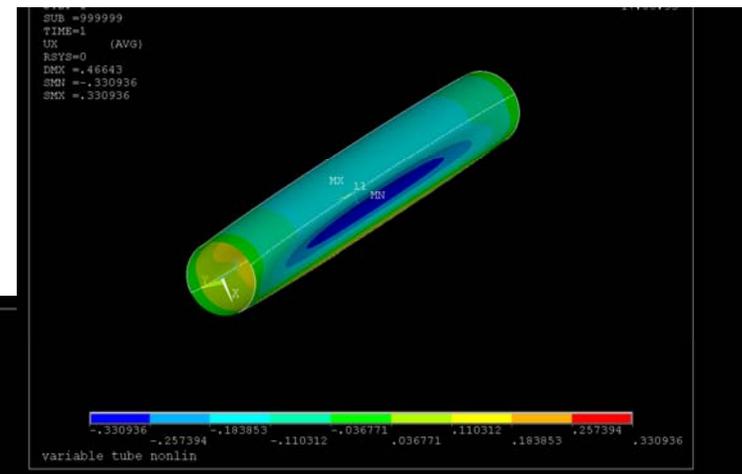
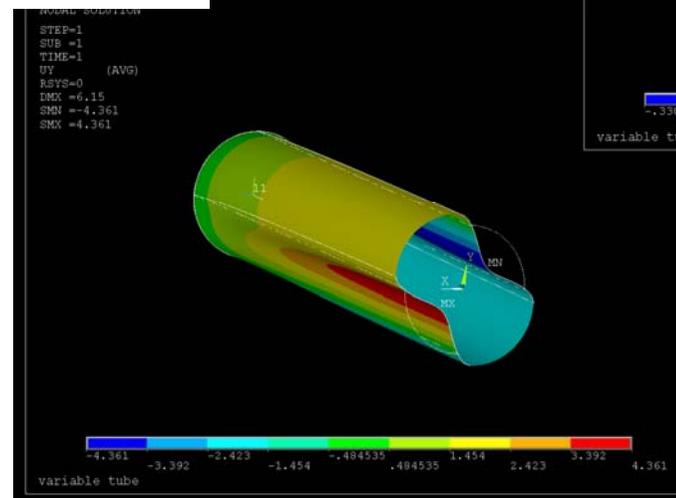
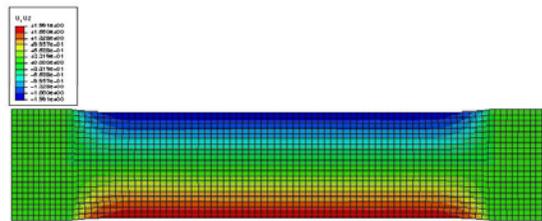
The Tensile tests are being used to calculate the material-properties of the developed material. For a range up to 3-5% strain standard methods can be used (approx. linear) e.g. rule of mixture / Hook's law

For strains above 5% different material-models are necessary: Fung, Holzapfel-Gasser-Ogden (Hyperelastic; anisotropic)

# Simulation

The calculated material-constants are used to simulate various geometries with Abaqus and Ansys using the Fung and Ogden models.

- Same geometry as the tensile-tests (verification)
- Tube-shaped (actuator-design)



## Conclusion / Outlook

Material- and production trials concluded a combination of pressure moulding and pultrusion with a TPE/Carbon material mix as the most suitable production process

Different TPE's should be tested with pultrusion to gauge range of mechanical properties

- Tests planned with Kraiburg TPE's Hipex<sup>®</sup>-material

Tensile tests showed expected results but also the necessity to improve the test methods

- further test are needed at different angles (to improve the data-base)
- tests in 0°-direction need to be improved
- Fatigue tests are needed

Simulation needs more refinement of the material-model

**Thank you for your attention!**

**Questions?**